

## ■ Supply air nozzle VŠ-4

### Application

VŠ-4 supply air nozzles are suitable for supplying either cold or warm air into rooms in applications requiring large throw distances and low noise levels. By arranging several nozzles in a block, the throw distance can be increased accordingly. Several installation methods are applicable.

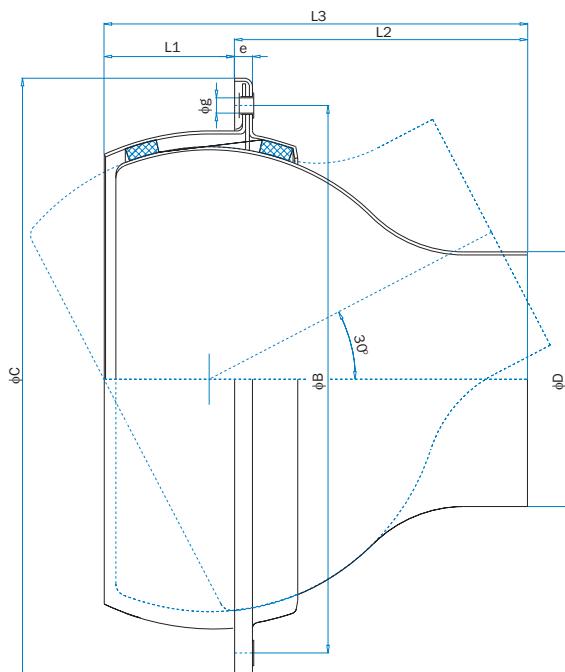


### Description

Supply air nozzles VŠ-4 are adjustable. The air jet injection can be adjusted either:

- manually within  $\pm 30^\circ$  in all directions or
- with electromotor within  $\pm 30^\circ$  in vertical or horizontal direction.

Adjusting depends on temperature oscillation. VŠ-4 supply air nozzles are made of anodised sheet aluminium. On customer's request, they can be powder painted in any of the RAL scale colours.

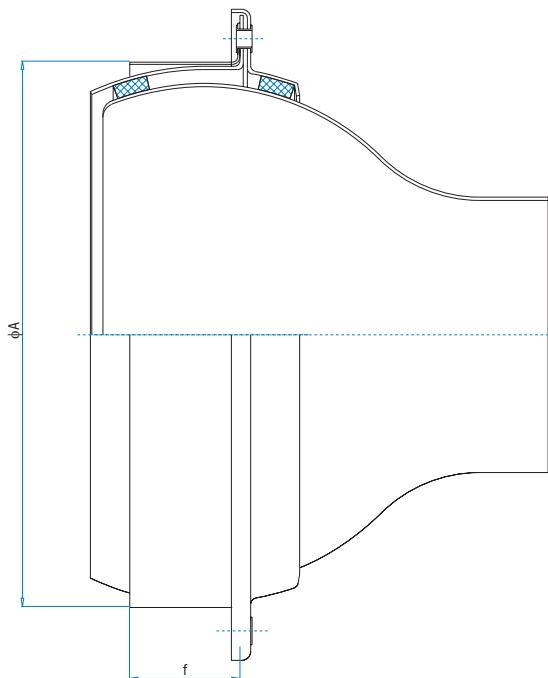


### Sizes and dimensions

Size	$\Phi D$	$\Phi B$	$\Phi c$	$e$	$L1$	$L2$	$L3$	$\Phi g$	n	$A_{ef} (m^2)$
<b>80</b>	80	175	196.5	7	43	96	139	6.5	3	0.004778
<b>100</b>	100	215	236.5	7	51	115	166	6.5	3	0.007543
<b>125</b>	125	265	286.5	7	52	142	194	6.5	3	0.011882
<b>160</b>	160	340	361.5	9	75	180	255	6.5	4	0.019607
<b>220</b>	220	425	446.5	9	95	219	314	6.5	4	0.037325

n – number of fixing boreholes

VŠ-4/E



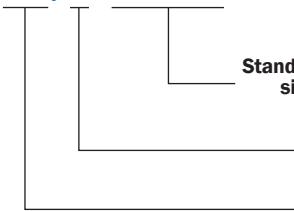
Size	$\Phi A$	f
80	158	40
100	198	40
125	248	40
160	313	40
220	398	65

**Installation methods**

- Mounting on a tube (marking **E**)

**Ordering key**

VŠ-4/ --- /R Size 125

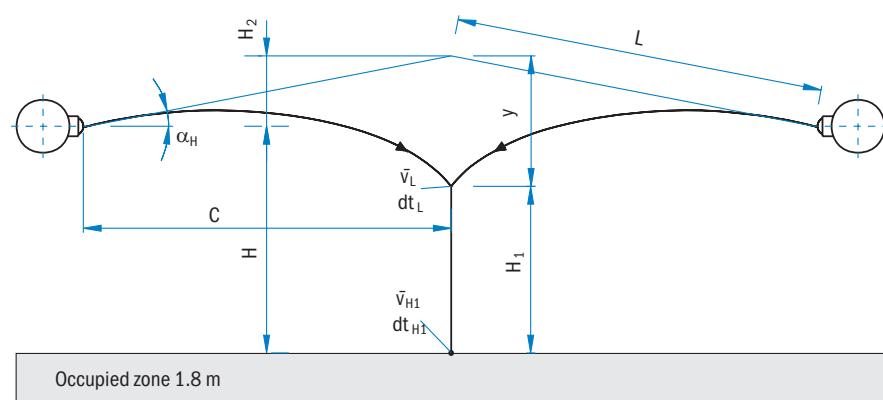
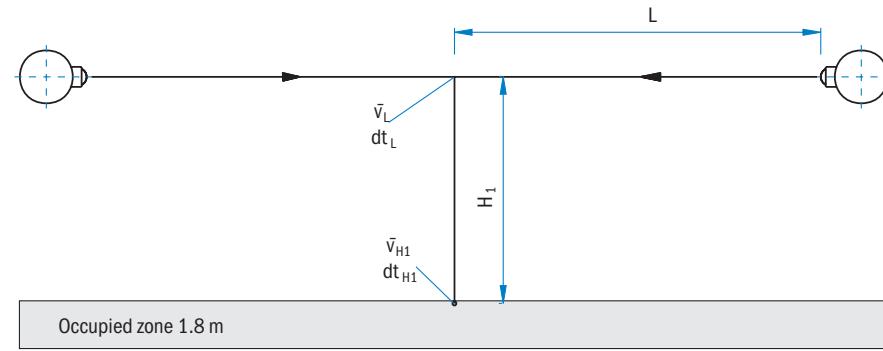
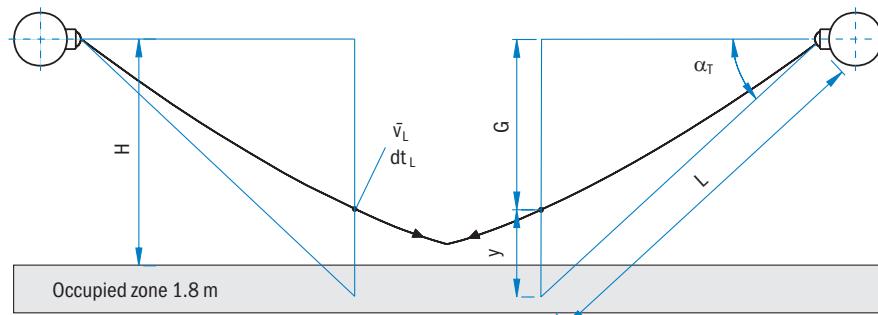


Standard sizes 80, 100, 125, 160, 220

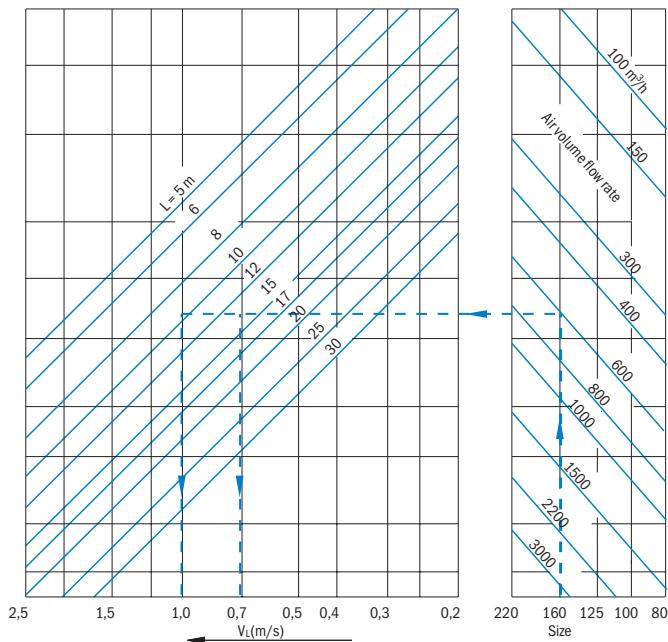
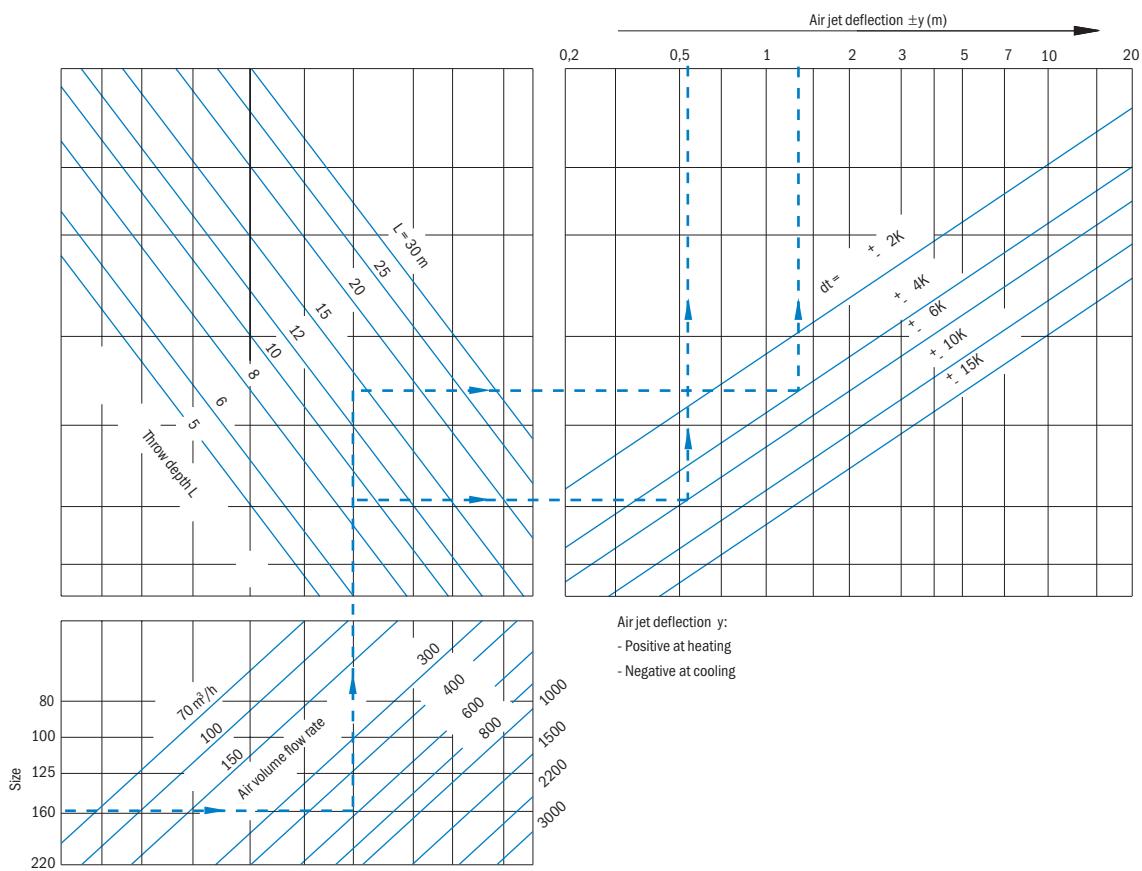
R Manual adjustment

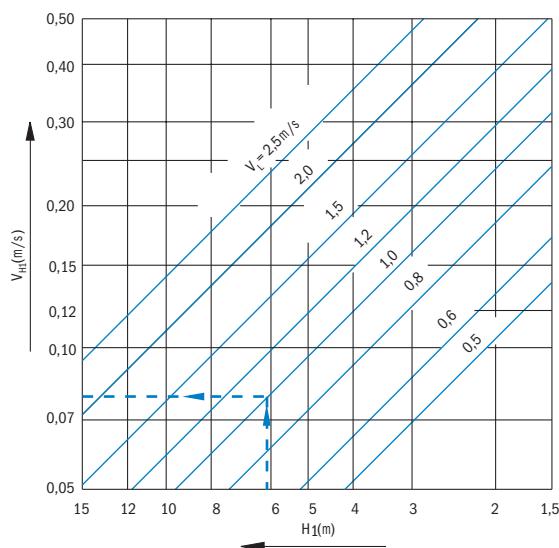
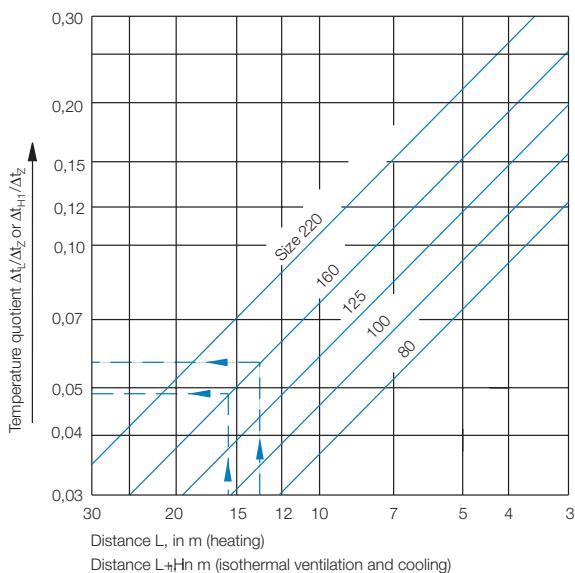
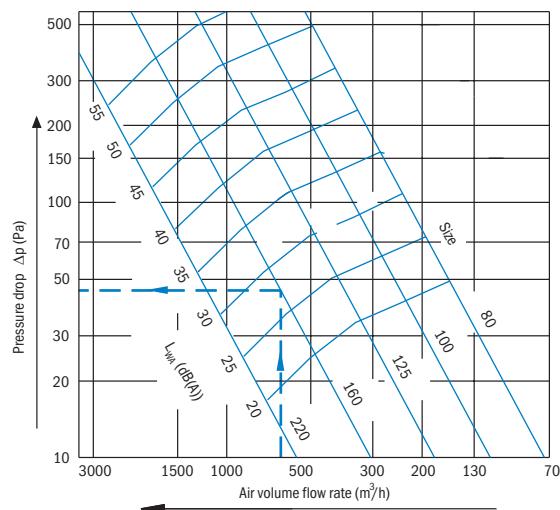
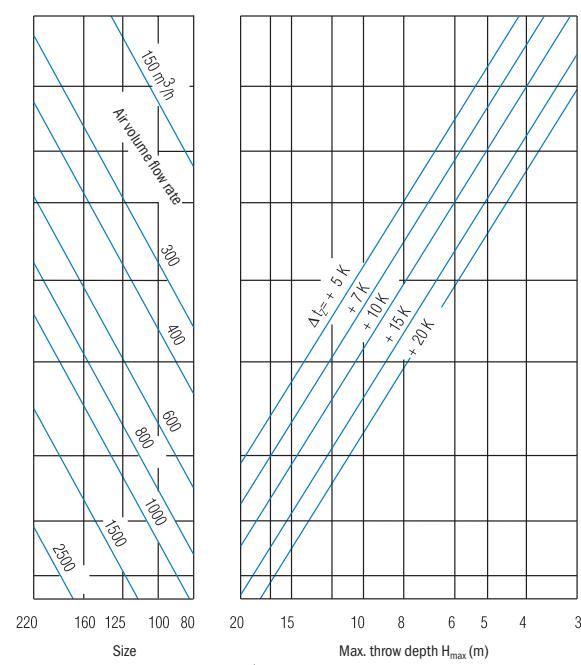
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E Mounting on a tube

**Cooling**

**Isothermal ventilation**

**Heating**

**Definition of symbols**

<b>L (m)</b>	Throw distance in isothermal condition
$\alpha_H$ (°)	Set angle in cooling mode
$\alpha_T$ (°)	Set angle in heating mode
<b>C (m)</b>	Horizontal distance between the nozzle and the two air jets collision point
<b>H (m)</b>	Height of the nozzle above the occupied zone
<b>H<sub>2</sub> (m)</b>	Virtual vertical distance between the nozzle and the two air jets collision point at isothermal air supply
<b>H<sub>max</sub> (m)</b>	Max. depth of air throw (only at vertical supply)
<b>H<sub>1</sub> (m)</b>	Vertical distance between the occupied zone and the two air jets collision point
<b>Y (m)</b>	Air jet deflection as a function of blow temperature difference
<b>G (m)</b>	Vertical distance between the air jet deflection point and the nozzle
$v_{H1}$ (m/s)	Average air velocity in the occupied zone $H_1$
$v_L$ (m/s)	Average air velocity at the two air jets collision point $L$
$dt_2$ (K)	Temperature difference between the supply air and the room air
$dt_L$ (K)	Temperature difference between the supply air at the distance $L$ and the room air
$dt_{H1}$ (K)	Temperature difference between the supply air at the entry in the occupied zone and the room air
$dp_t$ (Pa)	Total air pressure drop
$L_{WA}$ (dB(A))	Sound power level

**Diagram 1: Velocity in the air jet core and throw depth****Diagram 2: Air jet deflection**

**Diagram 3: Velocity at the air jet axis**

**Diagram 4: Temperature quotient**

**Diagram 5: Pressure drops and sound levels**

**Diagram 6: Maximum warm air throw depth at vertical supply**


### Calculation example

with regard to different air supply angles

#### Cooling ( $\alpha_{H1}$ )

- Select air supply angle ( $\alpha_{H1}$ ):
  - Calculate distance  $L$ :  $L = \frac{C}{\cos(\alpha_{H1})}$  (table 1)
  - Calculate height  $H_2$ :  $H_2 = \tan(\alpha_{H1}) \times C$  (table 1)
  - Select velocity  $v_L$  from diagram 1
  - Select air jet deflection  $y$  from diagram 2
  - Calculate height:  $H_1 = H + H_2 \cdot y$
  - Select velocity  $v_{H1}$  from diagram 3.
  - Select temperature quotient from diagram 4  $\frac{\Delta t_{H1}}{\Delta t_z}$  or  $\frac{\Delta t_L}{\Delta t_z}$ :
- $$\Delta t_{H1} = \frac{\Delta t_{H1}}{\Delta t_z} \times \Delta t_z \quad \Delta t_L = \frac{\Delta t_L}{\Delta t_z} \times \Delta t_z$$

### Calculation example

Isothermal ventilation

Apply diagram 1 and 3.

#### Heating ( $\alpha_T$ )

- Select velocity  $v_L$ .
- Select distance  $L$  from diagram 1.
- Establish air jet deflection  $y$  from diagram 2.
- Calculate air supply angle:

$$\sin(\alpha_T) = \frac{G+y}{L} \quad \text{table (1)}$$

- Select temperature quotient from diagram 4  $\frac{\Delta t_{H1}}{\Delta t_z}$  or  $\frac{\Delta t_L}{\Delta t_z}$ :
- $$\Delta t_{H1} = \frac{\Delta t_{H1}}{\Delta t_z} \times \Delta t_z \quad \Delta t_L = \frac{\Delta t_L}{\Delta t_z} \times \Delta t_z$$

#### Note:

In the case of the distance between nozzles smaller than  $0.14 \times C$ , velocity  $v_L$  and  $\Delta t_L$  are increased by a factor of  $\approx 1.5$

### Example

Two nozzles are installed at a distance of 18 m one from another and 7 m above the floor.

#### Air flow rate:

$V = 600 \text{ m}^3/\text{h}$  (per nozzle)

$\Delta t_z = -6\text{K}$  (summer)

$\Delta t_z = +4\text{K}$  (winter)

Selected: nozzle VŠ-4, size 160

#### Cooling: $(-\alpha_{Ht}) = 10^\circ$

- Distance  $L:L = c/\cos \alpha = 9/0.985 = 9.14 \text{ m}$  (table 1)
- Height  $H_2: H_2 = \tan(\alpha_{Ht}) \times 9 = 0.176 \times 9 = 1.578 \text{ m}$  (table 1)
- Select velocity  $v_L$  from diagram 1:  $v_L = 1.05 \text{ m/s}$
- Establish air deflection  $y$  from diagram 2:  $y = -0.6 \text{ m}$
- Calculate height  $H_1: H_1 = H + H_2 - y \quad H_1 = 5.2 + 1.587 - 0.6 = 6.187 \text{ m}$
- Select velocity  $v_{H1}$  from diagram 3:  $v_{H1} = 0.08 \text{ m/s}$
- Select temperature quotient from diagram 4  $\Delta t_{H1}/\Delta t_z$ :  
 $\Delta t_{H1} = \Delta t_{H1} / \Delta t_z \times \Delta t_z = 0.048 \times (-6) = -0.288 \text{ K}$

#### Heating: $(\alpha_t)$

- Select velocity  $v_L: v_L = 0.71 \text{ m/s}$
- Establish distance  $L$  from diagram 1:  $L = 13.5 \text{ m}$
- Establish air deflection  $y$  from diagram 2:  $y = +1.3 \text{ m}$
- Calculate air supply angle ( $\alpha_t$ ):  
 $\sin(\alpha_t) = G + y/L = 4 + 1.3/13.5 = 0.3926 \Rightarrow \alpha_t \approx 23^\circ$
- Select temperature quotient from diagram 4:

$$\Delta t_L = \frac{\Delta t_L}{\Delta t_z} \times \Delta t_z = 0.055 \times 4 = 0.22 \text{ K}$$

- From diagram 5, sound power level  $L_{WA}$  at the source can be established:  
 $L_{WA} = 27 \text{ dB(A)}$   
 $\Delta p_t = 43 \text{ Pa}$

**Table 1**

$\alpha_H$	$\cos(\alpha_H)$	$\tan(\alpha_H)$	$\alpha_t$	$\sin(\alpha_t)$
<b>0</b>	1	0	<b>0</b>	0
<b>5</b>	0.996	0.0875	<b>5</b>	0.087
<b>10</b>	0.985	0.176	<b>10</b>	0.174
<b>15</b>	0.966	0.268	<b>15</b>	0.260
<b>20</b>	0.940	0.364	<b>20</b>	0.342
<b>25</b>	0.906	0.466	<b>25</b>	0.423
<b>30</b>	0.866	0.577	<b>30</b>	0.500